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CRITERIA FOR EVALUATING THE EFFECTIVENESS OF THE "HYDRO TANK - COOLER" SYSTEM

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The energy lost in the control circuit turns into heat, increasing the temperature of the working fluid, which reduces its viscosity, increases the flow of leakage, and in turn is accompanied by a progressive increase in temperature due to the additional loss of escape energy.

An increase in temperature also leads to the oxidation of the working fluid and the formation of various deposits [1, 2].

q (Vt) with respect to [3] solving the equation - the thermal equivalent of the generated hydroelectric power. Volumetric transmission and absorption system, at a certain ambient temperature t_0^0 we have:

$$q = \frac{\sum_1^n k_i F_i}{1 - \exp\left\{-\frac{\sum_1^n k_i F_i}{\sum_1^n G_i c_i}\right\}} (t^0 - t_0^0), (1)$$

Here: e - the temperature of the working fluid at the outlet is a power-regulating complex (the temperature of the drain collector), deg.

In turn, $E(BT)$ lost in hydrostatic transmission [2] the thermal equivalent of the capacity will be:

$$E = rc_1 Q(t^0 - t_0^0) = Q\Delta P \frac{1-h}{h}, (2)$$

here t^0 - the temperature of the working fluid at the entrance to the "hydro tank - cooler" system is equal to the temperature of the working fluid at the output of the power control unit.

r - density of working fluid, kg / m³;

c_1 - the specific heat capacity of the working fluid is, J/ kg grad;

Q - working fluid output current, m³/ s;

ΔR - pressure drop in the hydraulic lines of the power control complex, Pa;

h - General efficiency of hydraulic circuit.



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Naturally, by updating the generated power plant surface miner, it is necessary to direct the lost power to the "hydro tank - cooler" system, for normal operation of the "hydro tank - cooler" system:

- $\mu \geq \mu_{\max}$ to maintain the viscosity coefficient in the surface miner's positive temperature range, the following condition must be met:

$$- \frac{q}{E} \geq 1,0; \quad (3)$$

The viscosity coefficient in the negative temperature range of the surface miner's work is $\mu \geq \mu_{\max}$ to hold inside, the following condition must be met:

$$\frac{N+E}{q} \geq 1,0, \quad (4)$$

Here N_H - tank heater power, Vt.

Notable [2] according to the equation, the power of the tank heater:

$$N_H = \sum_1^n k_i F_i \left(1 + \frac{1}{\ln \frac{t^0}{t_0^0}} \right) (t^0 - t_0^0) \quad (5)$$

- here t_0^0 - hydraulic machines of the surface miner's power control complex can operate without a heater the minimum temperature of the tank, grad.

In addition, considering that the duration of the temporary process is much less than the duration of the work cycle, for example, the surface miner we are considering, can be estimated with sufficient accuracy:

$$\text{Exp} \left\{ - \frac{\sum_1^n k_i F_i}{\sum_1^n G c_i} t \right\} \rightarrow 0,$$

then using the installed capacity of the full combine power plant pumps, equations (3) and (4) in the range of (2) and (5) positive operating temperature $t_{0\max}^0 \geq t_0^0 \geq 0^\circ\text{C}$ up to miner, they take the form

$$\frac{\sum_1^n k_i F_i}{[Q]_H [P]} \frac{h}{1-h} (t^0 - t_0^0) \geq 1,0; \quad (6)$$

here: $[Q]_H$ - nominal flow rate of working fluid of pumping station of power plant, m^3/s .

In turn, the surface miner's $t_{0\min}^0 \leq t_0^0 \leq 0^\circ\text{C}$ taking into account (2) and (5) in the range of negative working temperatures up to (3) and (4) the equations take the form:

$$\frac{(t^0 - t_0^0) \left(1 + \frac{1}{\ln \frac{t^0}{t_0^0}} \right) + \frac{[Q]_H [P] 1-h}{\sum_1^n k_i F_i h}}{t^0 - t_0^0} \geq 1,0. \quad (7)$$



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Analysis of equations (6) and (7) (graphic interpretation is presented in shows that they can be used as a criterion for temperature adaptation of the hydro tank - cooler system of a mining machine power plant. to evaluate posteriori already created cars. Previous studies [3, 4-11] show that the efficient and reliable operation of hydraulic mining machines is ensured by the practically efficient operation of the "hydro tank - cooler" system of the working fluid.

Therefore, even at the design stage of the machine, it is necessary to perform an entire line to assess its priority performance, which allows us to determine the rational parameters of the hydro tank – cooler system, research towards solving the urgent scientific problem of finding reasonable parameters of the hydraulic cooling tank system for modern and promising structures.

References

1. Bashta T.M. Mechanical engineering hydraulics. Reference, M., GNTI "mechanical engineering literature", 1963, 523 P. on.from.
2. Kovalevsky V.F. Thermal calculations of the hydraulic drive of heat exchangers and mining machines, M.: Nedra, 1972, 224
3. Mednikov N.N., Sytenkov V.N. Methodology for calculating the productivity of rotary excavators and milling combines in relation to technological schemes for the development of overburden rocks of a phosphorous quarry. Navoi NGGI // Gorny vestnik of Uzbekistan No. 1, 2001. pp. 88-91. 2.
4. Abduazizov N.A. Justification and choice of parameters of the "hydraulic tank cooler" system of a hydro-volumetric power plant of a quarry combine. Candidate of Dissertation M.: MGSU., 2008. 143s. with ill.
5. Brodsky G.S. Justification, selection of parameters and development of working fluid filtration systems for hydrofected mining machines. Abstract of the doct. diss. M.: MGSU., 2006, 44 p., ill. 4. Azamatovich N. et al. INVESTIGATION OF THE INFLUENCE OF THE AMOUNT OF CONTAMINATION OF THE WORKING FLUID ON THE RELIABILITY OF MINING MACHINES //RESEARCH AND EDUCATION. – 2022. – Vol. 1. – No. 8. – PP. 95-103.
6. Abduazizov N.A. Development of methods to improve the efficiency of quarry hydrofected excavators based on optimization of their hydraulic systems Uzbekistan // Dissertation of the Doctor of Technical Sciences. – Almalyk, 2020. – 200 p.
7. Abduazizov N. A., Sh Z. A. Development of the Mathematical Model of Thermal Processes in the Controlling Loop of the Hydraulic Power Unit of the Quarry



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Combine //International Journal of Advanced Research in Science, Engineering and Technology. India. – 2018. – Т. 5. – №. 9.

8. Абдуазизов Н. А. Повышение эффективности гидравлической системы карьерных экскаваторов //Монография.-Навои.–2020. – 2020.

9. Абдуазизов Н. А. и др. НАДЕЖНОСТЬ ГИДРОСИСТЕМ ГОРНЫХ МАШИН //Интернаука. – 2017. – №. 17. – С. 27-29.

10. Абдуазизов Н. А. и др. МАТЕМАТИЧЕСКИЕ УРАВНЕНИЯ В РЕГУЛИРУЮЩИХ КОНТУРАХ ГИДРООБЪЕМНЫХ ТРАНСМИССИЙ ГИДРАВЛИЧЕСКОГО ЭКСКАВАТОРА //Интернаука. – 2017. – №. 30. – С. 30-33.

11. Абдуазизов Н. А. и др. ПАРАМЕТРЫ НАГРУЖЕНИЯ ОСНОВНЫХ МЕХАНИЗМОВ ГИДРАВЛИЧЕСКОГО ЭКСКАВАТОРА ПРИ ОТРАБОТКЕ УСТУПА //WORLD SCIENCE: PROBLEMS AND INNOVATIONS. – 2018. – С. 191-194.



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